# Structural and Dielectric Properties of the Mn-Doped BaO-Nd<sub>2</sub>O<sub>3</sub>-4TiO<sub>2</sub> System

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**Abstract:** The effect of the  $Nd_2O_3$  and  $TiO_2$  ratios on the microstructure, dielectric properties and quality factor  $(Q.f_r)$  of the 1 wt% Mn-doped BaO-Nd<sub>2</sub>O<sub>3</sub>-4TiO<sub>2</sub> system were investigated. The samples sintered at various temperatures were analysed by field emission scanning electron microscopy (FESEM), X-ray diffraction (XRD) and a network analyser at 3 GHz. The grains of the  $Nd_2O_3$  poor composition MBN0.5T4 were more spherical, whereas the grains of the excess Nd<sub>2</sub>O<sub>3</sub> composition MBN1.5T4 were spherical and rod-like. The grains of the  $TiO_2$  poor composition MBNT4 and the  $TiO_2$  rich composition MBNT5 were more rod-like than spherical. The grain size increased with increasing sintering temperature. The  $BaNd_2Ti_5O_{14}$  phase was observed for compositions based on a BaO/Nd<sub>2</sub>O<sub>3</sub> = 1 ratio. The composition that deviated from the BaO/Nd<sub>2</sub>O<sub>3</sub> = 1 ratio was composed of a major phase,  $BaNd_2Ti_5O_{14}$ , with some secondary phases,  $Nd_2Ti_2O_7$  and  $BaTi_4O_9$ . The formation of the secondary phases affects the density, dielectric properties and quality factor of the Mn-doped BaO-Nd<sub>2</sub>O<sub>3</sub>- $4TiO_2$  system. The dielectric constant varies from 35-85 with different  $Nd_2O_3$  and  $TiO_2$  contents. Quality factor values of 4200 to 10500 (at 3 GHz) can be obtained by varying the  $Nd_2O_3$  and  $TiO_2$ contents.

Keywords: Mn, dielectric properties, quality factor, BaO-Nd<sub>2</sub>O<sub>3</sub>-4TiO<sub>2</sub>

**Abstrak:** Kesan nisbah  $Nd_2O_3$  and  $TiO_2$  ke atas mikrostruktur, sifat dielektrik dan, faktor kualiti (Q.f<sub>r</sub>) 1% berat Mn-dop BaO- $Nd_2O_3$ - $4TiO_2$  telah dikaji. Sampel yang disinter pada pelbagai suhu dianalisa dengan menggunakan mikroskop elektron imbasan (FESEM), teknik pebelauan sinar-X (XRD) dan penganalisis rangkaian pada 3 GH<sub>2</sub>. Butiran bagi sistem MBN0.5T4 yang kekurangan  $Nd_2O_3$  berbentuk sfera manakala butiran yang berlebihan kandungan  $Nd_2O_3$  berbentuk rod. Saiz butiran pula didapati meningkat dengan suhu persekitaran. Fasa  $BaNd_2Ti_5O_{14}$  terbentuk bagi sampel dengan nisbah  $BaO/Nd_2O_3 = 1$ . Selain daripada komposisi didapati sampel mengandungi fasa utama  $BaNd_2Ti_5O_{14}$  bersama fasa sekunder  $Nd_2Ti_2O_7$  dan  $BaTi_4O_9$ . Pembentukan Fasa sekunder mempengaruhi ketumpatan, sifat dielektrik dan faktor kualiti sistem Mn-dop  $BaO-Nd_2O_3$ -4 $TiO_2$ . Pemalar dielektrik berubah dari 35–85 dengan kandungan  $Nd_2O_3$  dan  $TiO_2$  yang berlainan. Faktor kualiti yang bernilai 4200 hingga 10500 (pada 3 GHz) boleh dicapai dengan mengubah kandungan  $Nd_2O_3$  dan  $TiO_2$ .

Kata kunci: Mn, sifat dielektrik, faktor kualiti, BaO-Nd<sub>2</sub>O<sub>3</sub>-4TiO<sub>2</sub>

# 1. INTRODUCTION

Modern microwave telecommunication systems require ceramic dielectric resonators (DR) that exhibit a high quality factor (Q  $\cong$  (tan  $\delta$ )<sup>-1</sup>) and relative permittivity ( $\varepsilon_r$ ) and a near-zero temperature coefficient of resonant frequency  $(\tau_f)$ .<sup>1,2</sup> Despite their technical importance and widespread use, only a very few ceramic materials are known that meet these stringent property requirements. In the early days, TiO<sub>2</sub> attracted substantial attention due to its high relative permittivity ( $\varepsilon_r \sim 100$ ) and high quality factor (Q.f<sub>r</sub> ~50000 at 3 GHz).<sup>3</sup> Subsequent development resulted in useful compounds in the BaO-TiO<sub>2</sub> system. One of the materials described as having practical applications as a DR was BaTi<sub>4</sub>O<sub>9</sub>, which has an  $\varepsilon_r \sim 38$  and Q.f<sub>r</sub>  $\sim 28160$  at 11GHz.<sup>4</sup> These results provoked exploration of materials in several BaO-M<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub> systems, where M is a rare earth species. The first system to be investigated was BaO-Nd<sub>2</sub>O<sub>3</sub>-TiO<sub>3</sub>. A later work by Kolar et al.<sup>5</sup> reported a compound with a molar ratio near BaO-Nd<sub>2</sub>O<sub>3</sub>.5TiO<sub>2</sub> that was identified as having practical microwave properties because it exhibited  $\varepsilon r \sim 77$  and Q.fr  $\sim 17600$ . It is generally accepted that the characteristics of BaO-Nd<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub> ceramics strongly depend on their crystal structure, stoichiometry, grain size, additives and phase composition.<sup>6-9</sup> Consequently, numerous approaches existed for modifying the characteristic of BaO-Nd<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub> including (1) doping with additives of SrO, PbO, Ta<sub>2</sub>O<sub>5</sub> and other rare earth oxides<sup>10-14</sup> and (2) varying the composition. As for this work, we have attempted to vary the composition by changing the ratio of Nd<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub> in 1 wt% Mn-doped BaO-Nd<sub>2</sub>O<sub>3</sub>-4TiO<sub>3</sub> system. The effects of compositional change upon the microstructure, dielectric properties and quality factor are reported in this study. Mn of 1 wt% was added to all the compositions in our experiment because, in our previous work, we acknowledged that Mn addition promotes densification of BaO-Nd<sub>2</sub>O<sub>3</sub>-4TiO<sub>3</sub> and enhances the quality factor of the system.<sup>15</sup>

### 2. EXPERIMENTAL

Samples were prepared by the conventional method using  $BaCO_3$ . TiO<sub>2</sub>, MnO and Nd<sub>2</sub>O<sub>3</sub> powders of high purity above 99.9% (Merck, Germany). The compositions investigated in this study are summarised in Table 1.

Sample	Composition
MBN0.5T4	$1BaO-0.5Nd_2O_3-4TiO_2$ with 1 wt% Mn
MBNT4	1BaO-1Nd <sub>2</sub> O <sub>3</sub> -4TiO <sub>2</sub> with 1 wt% Mn
MBN1.5T4	$1BaO-1.5Nd_2O_3-4TiO_2$ with 1 wt% Mn
MBNT5	$1BaO\text{-}1Nd_2O_3\text{-}5TiO_2$ with 1 wt% Mn

Table 1: Composition of the samples.

Mixing was carried out in a polyethylene bottle containing zirconia balls and deionised water. The mixture was calcined at 1150°C for 2 h, dried, crushed and then pressed with a cylindrical mould with a diameter of 16 mm under a pressure of 150 MPa to yield samples in pellet form. The specimens were sintered at various temperatures in the range of 1200°C to 1400°C for 2 h. The relative densities of the sintered samples were measured using a densitometer. Phase analysis was performed using a Bruker D8 powder diffractometer operating in reflection mode with Cu Ka radiation. Microstructure observation was conducted using a field emission scanning electron microscope (FESEM SUPRA 35VP ZEISS) operating at working distances down to 1 mm and an extended accelerating voltage range from 30 kV down to 100 V. Samples for  $\varepsilon_r$  and *Q.fr* measurements were prepared from sintered pellets by polishing both faces of the pellets with SiC paper (1000) followed by 0.1  $\mu$ m Al<sub>2</sub>O<sub>3</sub> paste. The  $\varepsilon_r$  and *Q.fr* were measured using a network analyser at 3 GHz.

### 3. **RESULTS AND DISCUSSION**

#### 3.1 Microstructure

Figure 1 shows the microstructures of sintered MBNT4 at different sintering temperatures ( $1250^{\circ}$ C,  $1300^{\circ}$ C and  $1350^{\circ}$ C). Both spherical and rod-shaped grains were observed in the sample sintered at  $1250^{\circ}$ C. The diameter of the spherical grains and rod-like grains are similar in the range of 0.5 to 0.8 µm. The lengths of the rod-like grains were of 2.0 to 2.5 µm. As the temperature was increased to  $1300^{\circ}$ C, the grains became slightly larger, with diameters of 1.0 to 1.2 µm. The lengths of the rod-like grains were approximately 2.0 to 4.0 µm. By increasing the sintering temperature to  $1350^{\circ}$ C, the spherical grains disappeared, and rod-like grains with diameters of 1.5 to 2.0 µm and lengths of 8.0 to 10.0 µm were observed. The change in the shape suggests that the grain growth occurs along orthorhombic a or b axes because these axes are longer than the c axis in the orthorhombic structure.

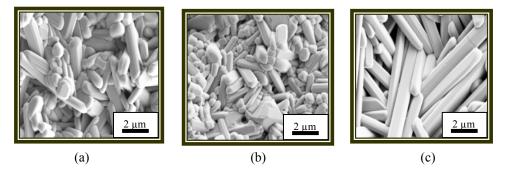


Figure 1: SEM micrographs of sintered MBNT4 at different sintering temperatures: (a) 1250°C, (b) 1300°C and (c) 1350°C.

Figure 2 shows the microstructures of the sintered samples  $(1300^{\circ}C, 2 h)$  with different compositions. Both spherical and rod-like grains were observed in all the samples. The grains of the Nd<sub>2</sub>O<sub>3</sub> poor composition MBN0.5T4 were mostly spherical with little rod-like structure. For the excess Nd<sub>2</sub>O<sub>3</sub> composition MBN1.5T4, the grains were mostly rod-like with little spherical structure. The shapes of the grains in MBNT4 comprised both spherical and rod-like, whereas the grains in the excess TiO<sub>2</sub> composition, MBNT5, were mostly rod-like. The grain sizes in MBN0.5T4 and MBNT4 were relatively small compared to those of MBN1.5T4 and MBNT5. This result is in agreement with the results reported by Chen et al<sup>11</sup> and Fu et al.<sup>16</sup>, in which they found that excess Nd<sub>2</sub>O<sub>3</sub> and excess TiO<sub>2</sub> promote grain growth.

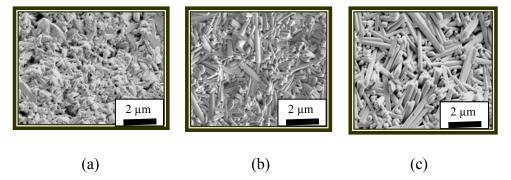


Figure 2: SEM micrographs of the sintered samples with different compositions: (a) MBN0.5T4, (b) MBN1.5T4 and (c) MBNT5.

#### 3.2 XRD Results

The corresponding XRD patterns of the four different compositions are shown in Figure 3. The patterns for all the compositions fit well with the orthorhombic phase of standard  $BaNd_2Ti_5O_{14}$  ICDD No 33–136. The lattice parameters of the XRD show a = 12.20 Å, b = 22.35 Å and c = 3.84 Å. However, detailed observation shows the presence of extra peaks in MBN0.5T4 and MBN1.5T4. The extra peaks in MBN0.5T4 and MBN1.5T4 were identified as  $BaTi_4O_9$  and  $Nd_2Ti_2O_7$ , respectively.  $Nd_2Ti_2O_7$  compounds may have formed because the excess  $Nd_2O_3$  reacted with TiO<sub>2</sub>, whereas  $BaTi_4O_9$  compounds may have formed because the  $BaTiO_3$  reacted with excess  $TiO_2$ . However, XRD peaks that correspond to MnO were not detected in any of the compositions, probably due to the small content of MnO in the samples.

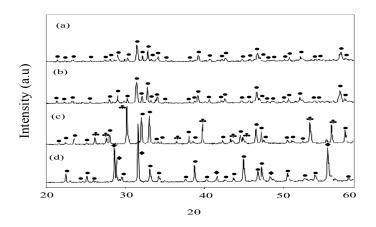


Figure 3: XRD patterns of the four different compositions: (a) MBNT5, (b) MBNT4, (c) MBN0.5T4 and (d) MBN1.5T4. [(•) BaNd<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub>. (•) Nd<sub>2</sub>Ti<sub>2</sub>O<sub>7</sub>. (•)BaTi<sub>4</sub>O<sub>9</sub>]

### 3.3 Density

Various factors influence the microwave properties of dielectric materials, including the contents of individual crystalline, secondary phases and the degree of densification. Therefore, a series of experiments was performed to find the optimum densification of each sample. Figure 4 presents the densities of MBNT4, MBNT5, MBN0.5T4 and MBN1.5T4 sintered at various temperatures for 2 h.

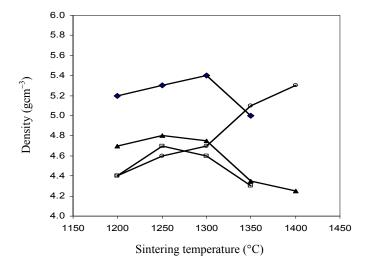


Figure 4: Densities of samples sintered at various temperature for 2 h. [(□) MBNT5, (♦) MBNT4, (▲) MBN0.5T4 and (O) MBN1.5T4].

The sintered density of MBNT5 was higher than MBNT4 at a given sintering temperature. This behaviour could be explained by considering the microstructure changes of MBNT5, which showed elongated grain and high porosity compared to MBNT4. MBNT5 showed a maximum density of 4.7 gcm<sup>-3</sup> at 1250°C, whereas MBNT4 showed a maximum density of 5.4 gcm<sup>-3</sup> at 1300°C. This result indicates that the excess TiO<sub>2</sub> in MBNT5 promotes densification at low temperature, and this might be due to the TiO<sub>2</sub> having a lower melting temperature than other oxides.<sup>16</sup> The density of the composition containing excess Nd<sub>2</sub>O<sub>3</sub> (MBN1.5T4) increased gradually with sintering temperature and showed a maximum density of 5.3 gcm<sup>-3</sup> at 1400°C, whereas the composition containing less Nd<sub>2</sub>O<sub>3</sub> (MBN0.5T4) shows a maximum density (4.8 gcm<sup>-3</sup>) at 1250°C, which declined as the sintering temperature increased. This result suggests that the composition containing more Nd<sub>2</sub>O<sub>3</sub> requires high temperature for interdiffusion of the Nd<sub>2</sub>O<sub>3</sub>, which has a high melting temperature, into a chemically and crystallographically uniform structure to attain maximum density.<sup>11</sup>

### 3.4 Dielectric Properties

Figure 5 shows the changes in dielectric constant at 3 GHz as a function of sintering temperature with different compositions. The sample with composition MBNT4 showed the highest dielectric constant in the range of 75 to 85 with different sintering temperatures. The value of the dielectric constant decreased by 50% as the TiO<sub>2</sub> content increased (MBNT5). Furthermore, the results also demonstrate that the sintering temperature to achieve maximum dielectric value decreased as TiO<sub>2</sub> increased. For example, the maximum dielectric of MBNT4 was 85, and it was attained at 1300°C, whereas for MBNT5, the maximum dielectric constant, 60, was obtained at 1250°C. The trend of this result indicates that the dielectric constant is closely related to the density changes in Figure 4. This can be explained by considering the capacitance of a porous sample and a dense sample. For the porous sample, the total capacitance comprises the capacitance of the grain and air in the pores. It is well known that the capacitance of air is very much less than that of the grains.<sup>17</sup> Therefore, the less dense sample has a lower dielectric constant than the dense sample. The composition containing excess Nd<sub>2</sub>O<sub>3</sub>, MBNT1.5T4, has a dielectric constant below 55, and the maximum dielectric constant was obtained at 1400°C. The composition containing less Nd<sub>2</sub>O<sub>3</sub>, MBNT0.5T4, has a dielectric constant below 60, and the maximum dielectric constant was obtained at 1250°C and 1300°C. In summary, the dielectric constants for the samples with compositions deviating from a BaO/Nd<sub>2</sub>O<sub>3</sub> = 1 ratio were relatively low, and this might be due to the presence of the secondary phase  $Nd_2Ti_2O_7$  and  $BaTi_4O_9$  compound.

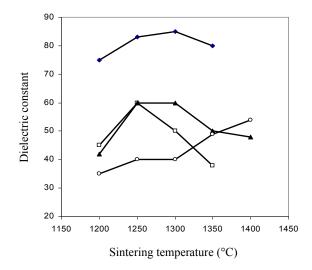


Figure 5: Dielectric of samples sintered at various temperature for 2 h. [(□) MBNTS,
(♦) MBN0.5T4, (▲) MBN0.5T4, (O) MBN1.5T4]

### 3.5 Quality Factor $(Q.f_r)$

The effect of sintering temperature on the Q.f<sub>r</sub> of Mn-doped BaO-Nd<sub>2</sub>O<sub>3</sub>-4TiO<sub>2</sub> is shown in Figure 6. As the proportion of TiO<sub>2</sub> increased in MBNT, the samples exhibited excellent Q.f<sub>r</sub> values. For example, the Q.f<sub>r</sub> of MBNT5 was in the range of 9000 to 10500, whereas for MBNT4, the Q.f<sub>r</sub> value was in the range of 7000–8500. The enhancement in the Q.f<sub>r</sub> value in MBNT5 is probably due to the fact that TiO<sub>2</sub> has a high Q.f<sub>r</sub> value. The composition containing less Nd<sub>2</sub>O<sub>3</sub> showed a higher Q.f<sub>r</sub> value than the composition containing excess Nd<sub>2</sub>O<sub>3</sub>. This fact could be explained by the existence of the secondary phase Nd<sub>2</sub>Ti<sub>2</sub>O<sub>7</sub> in MBN1.5T4, which is known to have a low Q value, and BaTi<sub>4</sub>O<sub>9</sub> compound in MBN0.5T4, which is known to have a high Q value.<sup>18</sup>

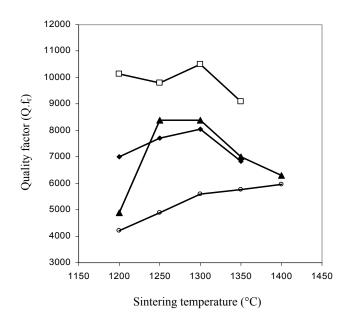


Figure 6: Quality factors of samples sintered at various temperatures for 2 h. [(□) MBNT5, (♦) MBNT4, (▲) MBNO. 5T4 and (O) MBN1.5T4.

#### 4. CONCLUSION

The Nd<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub> ratio control the density, dielectric constant, quality factor, phase and microstructure of 1 wt% Mn-doped BaO-Nd<sub>2</sub>O<sub>3</sub>-4TiO<sub>2</sub>. The proportions of spherical and rod-like grains depend on the composition and sintering temperature. The pure phase was obtained for a BaO/Nd<sub>2</sub>O<sub>3</sub> ratio = 1, and any deviation from this ratio causes the formation of secondary phases.

Excess  $Nd_2O_3$  in the composition increased the sintering temperature for a maximum density, whereas excess  $TiO_2$  decreased it. The dielectric constant was high for a BaO/Nd<sub>2</sub>O<sub>3</sub> ratio = 1 and deteriorated when the ratio deviated from 1 due to secondary phase formation. The value of the quality factor decreased as  $Nd_2O_3$  increased. In contrast, the quality factor value increased as  $TiO_2$  increased.

# 5. ACKNOWLEDGEMENTS

The author would like to thank Universiti Sains Malaysia for sponsoring this work under Short Term Grant 2008 (6035276) and MOSTI for sponsoring it under the eScience fund (6013357).

# 6. **REFERENCES**

- 1. Wersing, W. (1996). Microwave ceramics for resonators and filters. *Curr. Opin. Solid State Mater. Sci.*, 11, 715–731.
- Wakino, K., Nishikawa, T., Ishikawa, Y. & Tamura, H. (1990). Dielectric resonator materials and their application for mobile communication systems. *Br. Ceram. Trans.* 89, 39–43.
- 3. Moulson, A. J. & Herbert, J. M. (1990). *Electroceramics: Materials, properties and applications.* London: Chapman & Hall.
- Masse, D. J., Pucel, R. A., Readey, D. W., Maguire, E. A. & Hartwig, C. P. (1971). A new low-loss high K temperature-compensated dielectric for microwave applications. *Proc. IEEE*, 59, 1628–1632.
- 5. Kolar, D. & Suvorov, D. (1998). High permittivity microwave ceramics. *Eur. J. Solid State and Inorg. Chem.*, 32, 751–760.
- 6. Skapin, S., Kolar, D., Suvorov, D. & Samardzija, Z. (1998). Phase equilibria in the BaTiO<sub>3</sub>-La<sub>2</sub>TiO<sub>5</sub>-TiO<sub>2</sub> system. *J. Mater. Res.*, 13(5), 1327.
- Srimala, S., Ahmad, F. M. N., Zainal, A. A., Radzali, O., West, A. & Sinclair, D. (2007). Impedance spectroscopy of Ba<sub>0.9</sub>Sr<sub>0.1</sub>TiO<sub>3</sub> prepared by low temperature aqueous synthesis. *J. Mater. Sci.*, 42, 2492–2498.
- 8. Srimala, S., Ahmad, F. M. N., Zainal, A. A., Radzali, O. & West, A. (2008). Structural and electrical characteristic of crystalline barium titanate synthesized by low temperature aqueous method. *J. Mater. Process. Techno.*, 195, 171–177.
- Zhu, J., Lu, W., Lei, W. & Wan, S. (2009). Effects of SrTiO<sub>3</sub> additives on the structure and microwave dielectric properties of Ba<sub>4.2</sub>Sm<sub>9.2</sub>Ti<sub>18</sub>O<sub>54</sub> ceramics. *Ceram. Int.*, 35, 855–860.
- Pei, J., Yue, Z., Zhao, F., Gui, Z. & Li, L. (2009). Microstructure and dielectric properties control of Ba<sub>4</sub>(Nd<sub>0.7</sub>Sm<sub>0.3</sub>)<sub>9.33</sub> Ti<sub>18</sub>O<sub>54</sub> microwave ceramics. *Ceram. Int.*, 35, 253–257.

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- 11. Chen, X. M. & Yang, J. S .(1999). Dielectric characteristics of ceramics in BaO-Nd<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub>-Ta<sub>2</sub>O<sub>5</sub> system. *J. Eur. Ceram. Soc.*, 19, 139–142.
- 12. Nenasheva, E. A., Kartenko, N. F., Trubitsina, O. N., Matveichuk, V. F., Sibirtsev, S. N. & Gaidamaka, I. M. (2007). Tunability and microwave dielectric properties of BaO-SrO-Nd<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub> ceramics. *J. Euro. Ceram. Soc.*, 27, 2845–2848.
- 13. Chen, X. M., Lu, G. L., Yang, J. S. & Wu, Y. J. (1999). Some tungstenbronze compounds in the BaO-Nd<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub>-Ta<sub>2</sub>O<sub>5</sub> system. *J. Solid State Chem.*, 148, 438–441.
- 14. Wakino, K., Minai, K. & Tamura, H. (1984). Microwave characteristics of (Zr,Sn)TiO<sub>4</sub> and BaO-PbO-Nd<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub> dielectric resonators. *J. Am. Ceram. Soc.*, 67, 278.
- Srimala, S., Ahmad, F. M. N. & Chong, T. S (2007). Effect of Mn addition on structural and microwave dielectric properties of BaO-Nd<sub>2</sub>O<sub>3</sub>-5TiO<sub>2</sub> system. *Malaysian J. Microscopy*, 218–221.
- 16. Fu, Y. P., Liu, C. W., Lin, C. H. H. & Hsieh, C. K. (2005). Effect of TiO<sub>2</sub> ratio on BaO-Nd<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub> microwave ceramics. *Ceram. Inter.*, 31, 667–670.
- 17. Irvine, J. T. S., Sinclair, D. C. & West, A. R. (1990). Electroceramics: Characterisation by impedance spectroscopy. *Adv. Mater.*, 2, 132–138.
- 18. Wu, Y. J. & Chen, X. M. (1999). Modified  $Ba_{6-3x}Nd_{8+2x}Ti_{18}O_{54}$ microwave dielectric ceramics. *J. Eur. Ceram. Soc.*, 19, 123–1126.